

### **AMENDMENTS TO THE SPECIFICATION**

Please replace the paragraph beginning at page 4, line 1, with the following rewritten paragraph:

-- Seal 6 should preferably be made from a high chromium content steel alloy in order to keep the tensile strength as low as possible so as to facilitate deformation of the bush. In order to avoid scoring, a hard surface layer 29 will preferably have to be applied. At a channel diameter of for instance 22 mm, the wall thickness of the bush will be roughly 2 mm and the height about 10 mm. At other channel diameters these dimensions will also change proportionally. In addition, the sealing bush preferably has an over measure in its height of 0.4 to 1.0% and is placed for instance with a shrink fit of H7p6 (NEN 2807) in the flow channel. --

Please replace the paragraph beginning at page 6, line 23, with the following rewritten paragraph:

-- These drawbacks are at least partly obviated by the device ~~as according to claims 9, 10 and 11 as in the present invention where the structural components defining the transverse separating surface are formed by the manifold and nozzle, or where the nozzle is mounted on the manifold by means of a number of independently controllable connecting elements, or where a connecting plate is formed by a nut and bolt assembly.~~ --

Please replace the paragraph beginning at page 6, line 25, with the following rewritten paragraph:

-- The connection between manifold 2 and nozzle 3 is obtained with two, and preferably four independently controllable connecting elements. In the drawings 1 and 4 these take the form of a nut and bolt 10 assembly, wherein the nut is preferably formed by a clamp plate 11. Bolts 10 extend through an opening provided for this purpose in manifold 2, ~~screwed into the clamping plate 11 on the opposite side of the manifold 2. The clamping plates 11 in turn engage the shoulder part 28 of nozzle 3 and in a shoulder part 28 of nozzle 3. Nuts 10 engage on four clamp plates 11,~~ whereby nozzle 3 is clamped fixedly against manifold 2. --

Please replace the paragraph beginning at page 8, line 3, with the following rewritten paragraph:

-- Nozzle 3 comprises a number of transverse structural components 16, 17 mutually separated by a transverse separating surface 5'. The sealing between components 16 and 17 is likewise formed by a sealing element or sealing ring 18 which extends over transverse separating surface 5'. Sealing ring 18 lies in the corresponding recesses 29 and 30. A screw-in is applied to fixedly connect nozzle parts 16, 17. A known problem in the prior art which occurs here is that the mutual positioning is not predictable, which generally results in problems. --

Please replace the paragraph beginning at page 9, line 20, with the following rewritten paragraph:

-- These drawbacks are obviated with the measures according to ~~claim 17~~ the present invention where a sleeve extends over an expansion space in the gate. All wiring and all connection points are concealed from view by a metal construction. It is hereby no longer possible for mechanical damage to the wiring to occur during transport of the injection-moulding device and during assembly in the mould. Teflon is replaced by Kapton. This is resistant to higher temperatures. An additional advantage is that the insulating value of Kapton is very high. The outer diameter of the insulated wire is hereby considerably smaller. Because wiring and connection lie inside a metal construction, further protective hoses no longer have to be arranged. --

Please add the following new paragraph after the paragraph ending on line 27 of page 8:

-- Reference number 34 represents a fixation element that connects to the foremost nozzle part 16, as illustrated in Figure 2. Reference number 38 represents a cavity defined by a distal part of nozzle 3. The cavity 38 extends about the fixation element 34. Reference number 39 represents a cavity formed by the fixation element 34 and extends about the nozzle part 16. Additionally, as shown in Figure 1, the fixation element 34 makes contact with nozzle 3 on the larger outer diameter. In this way, the outflow opening of the cavity 38 is kept in line with the mould cavity 12 in spite of the thermal expansion of manifold 2, which causes the nozzle parts 16 and 17 to move radially with respect to their common axes. Thereby, in case of a possible leakage of plastic flowing to cavity 38, fixation element 34

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ensures that plastic will not flow further than the point of contact between the fixation element 34 and the nozzle 3. --